

AD-A046 464

OMNEMII INC VIENNA VA
RESEARCH ON MANNED SYSTEM DESIGN USING OPERATOR MEASURES AND CR--ETC(U)
JUL 77 E M CONNELLY
OTR-62-77-2

F/G 5/8

N00014-75-C-0810

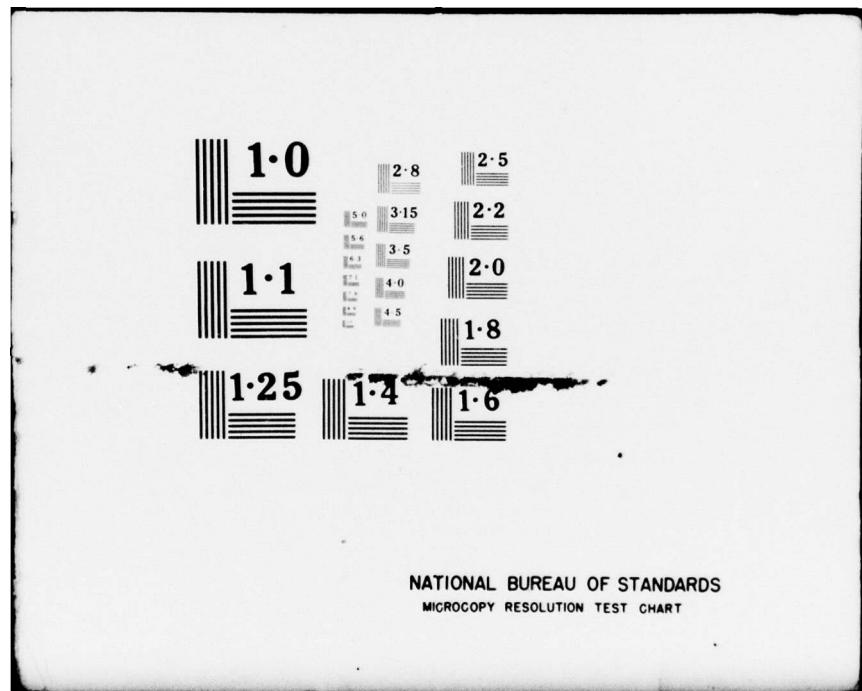
NL

UNCLASSIFIED

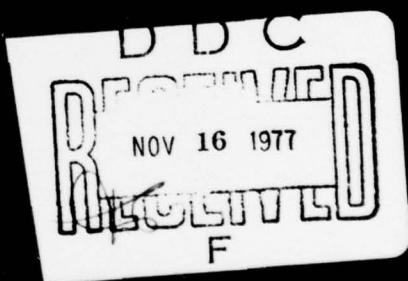
1 OF 1
ADA
046464



END
DATE
FILMED
12-77
DDC



ADA046464



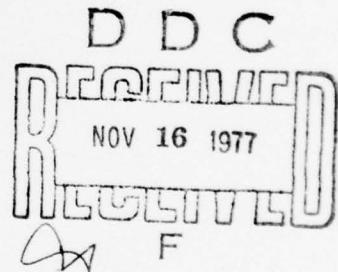
TECHNICAL REPORT NO. OTR-62-77-2
31 July 1977

(D)

FINAL REPORT

RESEARCH ON MANNED SYSTEM
DESIGN USING OPERATOR MEASURES
AND CRITERIA (OMAC) DATA

E. M. Connelly



This research was supported by the
Engineering Psychology Programs,
Office of Naval Research

Approved for Public Release; Distribution Unlimited

OMNEMII, INC.

P. O. Box 745
Vienna, Virginia 22180



703-938-5222

Unclassified

~~SECURITY CLASSIFICATION OF THIS PAGE~~ (When Data Entered)

DD FORM 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

391705

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

→ system performance models for ship control as an aid to ship display and control design.

A human operator model, which represents the total system response by identifying the criteria optimized by that response, was developed to represent the ship control performance of the Officer of the Deck (OOD). In addition, a sensitive contact (ship) avoidance measure was developed which detects conditions leading to ship collisions and near collisions. The OMAC and performance measure were used to demonstrate that significantly improved performance can be obtained with a new display design that automates information processing previously required of the OOD.

OMAC models representing performance obtained with each display design reveal that performance differences are explained by differences in a constraint self-imposed by the operator to select only a portion of the display information in order to control the ship. Constraint differences are equivalent to differences in the amount of information processed by the OOD with each display design. Further, the hypothesis that OOD participants using different displays attempt to perform according to invariant performance criteria was confirmed for superior performances. The hypothesis was not confirmed for less than superior performances.

EXPLANATION FOR		
3	White Section <input checked="" type="checkbox"/>	
4C	Buff Section <input type="checkbox"/>	
DETERMINING D		
STANDARDIZATION		
DISTRIBUTION AVAILABILITY CODES		
SP CIAL		
A		

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

TABLE OF CONTENTS

<u>SECTION</u>		<u>PAGE</u>
1.0	INTRODUCTION	1-1
2.0	MAJOR RESULTS OF THE RESEARCH	2-1
2.1	Contact Avoidance Performance Measurement	2-1
2.2	OMAC Modeling Concept	2-2
2.3	OMAC Representation of Operator Performances	2-4
2.4	OMAC Representation of Performance With OLD and PACS Displays	2-5
2.5	Representation of Human Performance by the OMAC Optimized	2-7
Reports Distributed		
References		
Distribution List		

ABSTRACT

In manned systems, performance can change significantly with changes in display design. With today's computer and display technology, it is possible to provide virtually any display function desired including automating many of the information processing tasks previously performed by the human operator. However, the relationship between display design and total system (people and machine) performance must be known in order to systematically select display features. The object of this research program was to investigate system performance models for ship control as an aid to ship display and control design.

A human operator model, which represents the total system response by identifying the criteria optimized by that response, was developed to represent the ship control performance of the Officer of the Deck (OOD). In addition, a sensitive contact (ship) avoidance measure was developed which detects conditions leading to ship collisions and near collisions. The OMAC and performance measure were used to demonstrate that significantly improved performance can be obtained with a new display design that automates information processing previously required of the OOD.

OMAC models representing performance obtained with each display design reveal that performance differences are explained by differences in a constraint self-imposed by the operator to select only a portion of the display information in order to control the ship. Constraint differences are equivalent to differences in the amount of information processed by the OOD with each display design. Further, the hypothesis that OOD participants using different displays attempt to perform according to invariant performance criteria was confirmed for superior performances. The hypothesis was not confirmed for less than superior performances.

INTRODUCTION

This report is the final report on contract number N00014-75-C-0810 between Omnimii, Inc. and Engineering Psychology Programs, Office of Naval Research. The contract was initiated on 1 April 1975 and completed on 30 May 1977.

The objectives of the research were to:

1. Develop a ship display/control design tool which would permit a designer to select alternative display features based on their effect on system performance.
2. Develop a method of representing operator control actions and resulting ship responses by the criteria optimized by those ship responses. This type of model is called "operator measures and criteria" (OMAC) model.
3. Devise a method of using the OMAC model to predict operator control actions and resultant ship responses in a variety of problem situations.
4. Develop a sensitive measure of contact (ship) avoidance performance.

This research program used data which had been previously collected during a series of experiments in which participants acting as Officer of the Deck (OOD) controlled a simulated ship in a simulated environment. The task was to direct a ship transit from the initial point to the terminal point within a pre-specified time interval while avoiding simulated contacts along the way. The experiment, using equipment known as the Surface Ship Bridge Console System (Beary; Gawitt), was run by personnel of NSRDC, Annapolis, Maryland, for purposes other than this research program. The data from that experiment were used in the research reported here.

Reports describing the research are listed in the section on reports distributed. Results of the research are summarized in the following paragraphs.

2.0 MAJOR RESULTS OF THE RESEARCH

2.1 Contact Avoidance Performance Measurement

Performance of manned systems is typically measured with summary measures, i.e., measures that summarize performance over the total simulated or actual mission. Examples of such measure components applied to ship control are:

1. Transit time;
2. Average deviation from a reference course;
3. Number of collisions or near collisions;
4. Fuel efficiency; and
5. Number of course and speed changes.

These components are usually weighted and summed to form the composit summary measure. However, such summary measures did not reveal the performance differences that existed with different displays tested in the ship control experiments referred to previously. Fortunately, a sensitive contact avoidance measure was developed as part of the research on this program to identify OMAC's that represent operator performances. With this measure, the performance differences with different displays were revealed.

Of importance here is not only discovery of improved performance with the advanced displays, but also the development of the sensitive contact avoidance performance measure. The success of

the measure supports the measurement principle: measures that detect responses leading to a critical condition (a ship collision) are more sensitive than measures that detect only the critical condition.

2.2 OMAC Modeling Concept

Performance prediction models have long been sought to aid in system design and to better understand how display designs affect performance. Present modeling methods (Connelly; Kleinman; McRuer; Preyss; Sheridan) which typically represent the human operator's moment-to-moment control response, have not provided the necessary predictive models. There are several difficult problems to overcome. One problem is that performance models should be applicable to operational or near operational settings and not limited to laboratory problems. Operational settings frequently require non-linear operator response functions - thus prohibiting the use of linear models. Another problem is that prediction of human response or human controlled system response on a moment-by-moment basis does not permit prediction of present response based on present conditions and the anticipated or planned activity by the operator. The modeling method used in the analysis reported here employs a construct based on optimal control theory to provide performance prediction.

Optimal control theory provides a means for determining the system response which, within the constraints imposed, is best according to the specified criteria. Given criteria and constraints, optimal control theory permits evaluation of all possible responses that satisfy the constraints, and in doing so identified the response that is best according to the criteria. Its property of interest here is that it relates system responses to criteria and vice versa. With this capability, it is possible to model a response by identifying the criteria optimized. This modeling process is the inverse of the process used by the designer of an automatic control system wherein criteria are selected first followed by determination of system responses that optimize those criteria. The inverse process used in this study starts with observed responses and seeks to identify the criteria optimized by these responses.

For manned systems, the OMAC criteria found to be optimized by observed responses should be distinguished from task criteria typically established by the system designer to specify desired system performance. While the OMAC criteria and the task criteria may be identical or similar, they are not necessarily the same; differences would reflect a lack of mutual understanding of task performance requirements. Also regarding manned systems, constraints can be imposed by the equipment (e.g., limited rudder deflection) or imposed by the operator (e.g., use of only a portion of the display information).

The control task considered here is a ship control problem where the OOD is to direct the ship from a starting location to an objective location and arrive at the objective in 90 minutes. The ship is to be controlled so as to avoid all contacts (other ships) by at least 3.70 kilometers (2 nautical miles). A task performance measure for this problem was developed using measures of transit time and contact avoidance. This task measure penalizes for excessive transit time and for passing contacts closer than 3.70 kilometers (2 nautical miles). The ship control involves equipment constraints such as an upper limit to speed and a lower limit to turning radius. Using the OMAC criteria analysis described, ship transiting responses which included contact avoidance maneuvering were modeled by the criteria optimized.

2.3

OMAC Representation of Operator Performances

OMAC's were identified for each operator performance. The ability of the OMAC's to represent individual performances was shown to be a function of the level of operator performance, i.e., superior performers were represented more accurately than were less skillful performers. In spite of difference in accuracy of representation, the representation is sufficiently accurate to permit prediction of operator performance, i.e., prediction of operator performance using OMAC's in a statistically significant manner.

A major result of the research was that for the ship control problem considered, OMAC must include both the criteria optimized and a purview constraint. Without both criteria and constraint, accurate modeling was not possible. The purview constraint found useful in the OMAC model represents a radius from own ship within which all contacts are considered. Contacts outside that radius are not considered for ship control. Other constraints such as considering a limited number of contacts may be useful but some type of purview function is necessary.

2.4

OMAC Representation of Performance With OLD and PACS Displays

OMAC's representing operator performance with two different display types (OLD and PACS¹) for two population groups (all participants and superior participants) were identified. From the results, several conclusions were possible.

1. A greater proportion of the performers were rated superior with the PACS display than with the OLD display. This suggests that with the PACS display there would be more superior performers in the general OOD population.

2. Superior performers with PACS and OLD displays are represented by the same OMAC criteria (the relative weighting

¹ OLD display is a conventional radar PPI display, PACS (Possible Area of Collision) is an advanced display that provides among other features the locus of collisions with all contacts for all possible own ship courses.

between contact avoidance and transit time). The average performance level with the two displays is different but the criteria optimized are the same. This suggests that consistent "target" criteria (the criteria sought by the operator) were the goal of superior performers with both displays; but, the operators were better able to reach that performance goal with the PACS display. This result suggests that the "target" criteria might be used in training where operators could be rated not only on performance but also on the criteria they apparently optimize.

3. Performance differences with different display types obtained from the superior performances are explained by a difference in purview (the range from own ship within which the operator processes contact data). The logic is: OMAC predicts operator performance; OMAC has two parts: criteria and purview; but, the criteria are constant while purview changes with changes in display. Indeed, the OMAC performance data show clearly the effect of purview on performance.

4. The purview rating for the OLD display was found to be 17.77 kilometers (9.6 nautical miles) while the PACS display was found to be 22.22 kilometers (12 nautical miles). Purview rating may be a function of contact density and thus the ratings given should not be considered absolute; but, only apply for the experimental control task.

5. The average number of contacts within purview in the experimental problem was a linear function of purview area. Thus, OOD ship handling performance may be a function of the number of contacts that the OOD can process with a given display design. If a display feature automates one or more information processing tasks, the OOD may be able to process more contacts, thus expanding his purview. According to the results discussed above (3), this would result in improved performance. This logic suggests that an analysis of the information processing required of the OOD per contact may permit direct prediction of OOD ship handling performance.

2.5

Representation of Human Performance by the OMAC Optimized

Based on the overall results obtained with the OMAC, it is concluded that the criteria modeling approach offers a practical way to model human performance in an operational or near operational problem setting. The generality of the method to other manned system problems should be investigated.

With this modeling method, the operator's output at each instant of time is represented by taking into account both the instantaneous problem state and planned operator outputs as a result of projections of controlled device responses. Projections of controlled device responses are the expected future responses of the device(s) or expected behavior of disturbing factors such as the contacts of the ship control problem.

Representative OMAC's reveal the target criteria of the human controller and permit evaluation of the ability to perform according to those criteria. OMAC's also reveal the constraints that may be self-imposed or are inherent, but which limit the operator's performance level.

OMAC's can be developed for individuals working with complex and non-linear tasks. The complexity of the task or the device being controlled does not limit the identification of the apparent OMAC.

REPORTS DISTRIBUTED

Connelly, E. M. and Sloan, N. A., Manned system design using operator measures and criteria (Technical Report OTR-62-76-1) Vienna, VA: Omnemii, Inc., October 1976. (AD A032687)

Connelly, E. M., Manned system performance as a function of display characteristics (Technical Report OTR-62-77-1) Vienna, VA: Omnemii, Inc., 31 July 1977.

Connelly, E. M., Manned system design using operator measures and criteria. Proceedings of the 21st Annual Meeting of the Human Factors Society, San Francisco, California, 18-20 October 1977.

REFERENCES

- Beary, Jr., Alexander D. The collision avoidance systems of the U. S. Navy surface ship bridge control console, Proceedings of the Fourth Ship Control Systems Symposium, Royal Netherlands Naval College, Den Helder, The Netherlands, October 27-31, 1975.
- Connelly, E. M. Development of a continuous performance measure for manual control (Final Report) Wright-Patterson AFB, OH: Omnimii, Inc., April 1977. (AMRL-TR-76-24)
- Gawitt, M. A. Surface ship bridge control system. Proceedings of the Fourth Ship Control Systems Symposium, Royal Netherlands Naval College, Den Helder, The Netherlands, October 27-31, 1975.
- Kleinman, D. L. & S. Baron. Application of optimal control theory to the prediction of human performance in a complex task, Technical Report AFFDL-TR-69-81) Wright-Patterson AFB, OH: Air Force Flight Dynamics Laboratory, March 1970.
- McRuer, D. & D. Graham. Human pilot dynamics in compensatory systems - theory models and experiments with controlled element and forcing function variations, (Technical Report AFFDL-TR-65-15) Wright-Patterson AFB, OH: Air Force Flight Dynamics Laboratory, 1965.
- Preyss, A. E. A theory and model of human learning behavior in a manual control task (Technical Report NASA CR-1124), 1968.
- Sheridan, T. B. & W. R. Ferrell. Man-machine systems: information, control, and decision models of human performance. Cambridge: MIT Press, 1974.

DISTRIBUTION LIST

Director, Engineering Psychology Programs, Code 455 Office of Naval Research 800 North Quincy Street Arlington, VA 22217 (5 cys)	Commanding Officer ONR Branch Office ATTN: Dr. J. Lester 495 Summer Street Boston, MA 02210
Defense Documentation Center Cameron Station Alexandria, VA 22314 (12 cys)	Commanding Officer ONR Branch Office ATTN: Dr. Charles Davis 536 South Clark Street Chicago, IL 60605
Dr. Robert Young Director, Cybernetics Technology Office Advanced Research Projects Agency 1400 Wilson Boulevard Arlington, VA 22209	Commanding Officer ONR Branch Office ATTN: Dr. E. Gloye 1030 East Green Street Pasadena, CA 91106
Col. Henry L. Taylor, USAF OOD(E&LS) ODDR&E Pentagon, Room 3D129 Washington, D. C. 20301	Commanding Officer ONR Branch Office ATTN: Mr. R. Lawson 1030 East Green Street Pasadena, CA 91106
Office of Naval Research International Programs Code 102IP 800 North Quincy Street Arlington, VA 22217 (6 cys)	Dr. M. Bertin Office of Naval Research Scientific Liaison Group American Embassy, Room A-407 APO San Francisco 96503
Director, Weapons Technology Programs, Code 212 Office of Naval Research 800 North Quincy Street Arlington, VA 22217	Director, Naval Research Laboratory Technical Information Division Code 2627 Washington, D. C. 20375 (6 cys)
Director, Physiology Program Code 441 Office of Naval Research 800 North Quincy Street Arlington, VA 22217	Mr. John Hill Naval Research Laboratory Code 5707.40 Washington, D. C. 20375

Office of the Chief of Naval Operations, OP987P10
Personnel Logistics Plans
Department of the Navy
Washington, D. C. 20350

Mr. Arnold Rubinstein
Naval Material Command
NAVMAT 0344
Department of the Navy
Washington, D. C. 20360

Commander
Naval Air Systems Command
Human Factors Programs, AIR 340F
Washington, D. C. 20361

Commander
Naval Air Systems Command
Crew Station Design, AIR 5313
Washington, D. C. 20361

Mr. T. Momiyama
Naval Air Systems Command
Advance Concepts Division,
AIR 03P34
Washington, D. C. 20361

Commander
Naval Electronics Systems Command
Human Factors Engineering Branch
Code 4701
Washington, D. C. 20360

LCDR T. W. Schropp
Naval Sea Systems Command
NAVSEA OOC-DA
Washington, D. C. 20362

Mr. James Jenkins
Naval Sea Systems Command
Code 06H1-3
Washington, D. C. 20362

Dr. James Curtin
Naval Sea Systems Command
Personnel & Training Analyses Office
NAVSEA 074C1
Washington, D. C. 20362

LCDR R. Gibson
Bureau of Medicine & Surgery
Aerospace Psychology Branch
Code 513
Washington, D. C. 20372

CDR Paul Nelson
Naval Medical R&D Command
Code 44
Naval Medical Center
Bethesda, MD 20014

Director
Behavioral Sciences Department
Naval Medical Research Institute
Bethesda, MD 20014

Dr. George Moeller
Human Factors Engineering Branch
Submarine Medical Research Laboratory
Naval Submarine Base
Groton, CT 06340

Mr. Phillip Andrews
Naval Sea Systems Command
NAVSEA 0341
Washington, D. C. 20362

Bureau of Naval Personnel
Special Assistant for Research Liaison
PERS-OR
Washington, D. C. 20370

Navy Personnel Research and
Development Center
Management Support Department
Code 210
San Diego, CA 92152

Dr. Fred Muckler
Navy Personnel Research and
Development Center
Manned Systems Design, Code 311
San Diego, CA 92152

LCDR Micheal O'Bar
Navy Personnel Research and
Development Center
Code 305
San Diego, CA 92152

Mr. A. V. Anderson
Navy Personnel Research and
Development Center
Code 302
San Diego, CA 92152

LCDR P. M. Curran
Human Factors Engineering Branch
Crew Systems Department, Code 4021
Naval Air Development Center
Johnsville
Warminster, PA 18950

LCDR William Moroney
Human Factors Engineering Branch
Code 1226
Pacific Missile Test Center
Point Mugu, CA 93042

Mr. Ronald A. Erickson
Human Factors Branch
Code 3175
Naval Weapons Center
China Lake, CA 93555

Human Factors Section
Systems Engineering Test Directorate
U.S. Naval Air Test Center
Patuxent River, MD 20670

Human Factors Division
Naval Ocean Systems Center
Department of the Navy
San Diego, CA 92152

Human Factors Engineering Branch
Naval Ship Research and Development
Center, Annapolis Division
Annapolis, MD 21402

Commanding Officer
Naval Coastal Systems Laboratory
Panama City, FL 32401

Dr. Robert French
Naval Ocean Systems Center
San Diego, CA 92132

Dr. Jerry C. Lamb
Display Branch
Code TD112
Naval Underwater Systems Center
New London, CT 06320

Naval Training Equipment Center
ATTN: Technical Library
Orlando, FL 32813

Human Factors Department
Code N215
Naval Training Equipment Center
Orlando, FL 32813

Dr. Alfred F. Smode
Training Analysis and Evaluation Group
Naval Training Equipment Center
Code N-OOT
Orlando, FL 32813

Dr. Gary Poock
Operations Research Department
Naval Postgraduate School
Monterey, CA 93940

Dr. A. L. Slafkosky
Scientific Advisor
Commandant of the Marine Corps
Code RD-1
Washington, D. C. 20380

Mr. J. Barber
Headquarters, Department of
the Army, DAPE-PBR
Washington, D. C. 20546

Dr. Joseph Zeidner
Director, Organization and
Systems Research Laboratory
U.S. Army Research Institute
5001 Eisenhower Avenue
Alexandria, VA 22333

Technical Director
U.S. Army Human Engineering Labs
Aberdeen Proving Ground
Aberdeen, MD 21005

U.S. Army Aeromedical
Research Lab
ATTN: CPT Gerald P. Krueger
Ft. Rucker, Alabama 36362

U.S. Air Force Office of
Scientific Research
Life Sciences Directorate, NL
Bolling Air Force Base
Washington, D. C. 20332

Dr. Donald A. Topmiller
Chief, Systems Engineering Branch
Human Engineering Division
USAF AMRL/HES
Wright-Patterson AFB, OH 45433

Lt. Col. Joseph A. Birt
Human Engineering Division
Aerospace Medical Research Lab
Wright-Patterson AFB, OH 45433

Air University Library
Maxwell Air Force Base, AL 36112

Dr. Robert Williges
Human Factors Laboratory
Virginia Polytechnic Institute and
State University
130 Whittemore Hall
Blacksburg, VA 24061

Mr. Alan J. Pesch
Eclectech Associates, Inc.
Post Office Box 179
North Stonington, CT 06359

Dr. W. S. Vaughan
Oceanautics, Inc.
422 6th Street
Annapolis, MD 21403

Dr. Arthur I. Siegel
Applied Psychological Services, Inc.
404 East Lancaster Street
Wayne, PA 19087

Dr. Robert R. Mackie
Human Factors Research, Inc.
Santa Barbara Research Park
6780 Cortona Drive
Goleta, CA 93017

Dr. Gershon Weltman
Perceptronics, Inc.
6271 Variel Avenue
Woodland Hills, CA 91364

Dr. Edward R. Jones
McDonnell-Douglas Astronautics
Company-EAST
St. Louis, MO 63166

Dr. Ross L. Pepper
Naval Ocean Systems Center
Hawaii Laboratory
P. O. Box 997
Kailua, Hawaii 96734

Dr. Meredith Crawford
5606 Montgomery Street
Chevy Chase, MD 20015

Dr. G. H. Robinson
University of Wisconsin
Department of Industrial Engineering
1513 University Avenue
Madison, WI 53706

Dr. Robert G. Pachella
University of Michigan
Department of Psychology
Human Performance Center
330 Packard Road
Ann Arbor, MI 48104

Dr. Jesse Orlansky
Institute for Defense Analyses
400 Army-Navy Drive
Arlington, VA 22202

Dr. Stanley Deutsch
Office of Life Sciences
HQS, NASA
600 Independence Avenue
Washington, D. C. 20546

Journal Supplement Abstract Service
American Psychological Association
1200 17th Street, N. W.
Washington, D. C. 20036 (3 cys)

Dr. William A. McClelland
Human Resources Research Office
300 N. Washington Street
Alexandria, VA 22314

Dr. William R. Utta!
University of Michigan
Institute for Social Research
Ann Arbor, MI 48106

Dr. Thomas B. Sheridan
Massachusetts Institute of Technology
Department of Mechanical Engineering
Cambridge, MA 02139

Dr. H. McIlvaine Parsons
Institute for Behavioral Research
2429 Linden Lane
Silver Spring, MD 20910

Director, Human Factors Wing
Defense and Civil Institute of
Environmental Medicine
Post Office Box 2000
Downsville, Toronto, Ontario
CANADA

Dr. A. D. Baddeley
Director, Applied Psychology Unit
Medical Research Council
15 Chaucer Road
Cambridge, CB2 2EF
ENGLAND